

# Cylindrical Straight Slab Type Gas Laser

## Background of the Invention

The present invention relates to a slab type gas laser, more specifically to a construction to provide an excellent laser beam having substantially Gaussian distribution in focussed output laser beam profile.

A slab type gas laser is known as one type of gas lasers such as C O<sub>2</sub> (carbon dioxide) laser. In a slab type gas laser, the gap between excitation electrodes is narrow so that the excited gas colliding with the electrodes is cooled, thereby accelerating the release of laser lower level. This is the reason why the laser is known as an electrode diffusion cooling type laser.

The slab type gas laser is classified into a waveguide type laser and a straight type laser depending on the way how the light propagates. In the waveguide type laser including a C O<sub>2</sub> laser of 10  $\mu$  m emission wavelength, the gap between two electrodes is in the order of approximately several mm. The laser beam propagates in the waveguide mode by being reflected between the electrodes in a zigzag manner. On the other hand, in the straight type gas laser, the gap between the electrodes is large enough so that the light can propagate in the free space. As a result, the light propagates between the electrodes in a free space mode.

A known cylindrical straight slab type gas laser comprises a pair of cylindrical electrodes of different diameter disposed horizontally and concentrically. The gap between the two cylindrical electrodes is filled with laser medium to define a cylindrical straight slab. A ring-shaped mirror is disposed at one end of the cylindrical straight slab and an output mirror is disposed at the center of the one end to pass a part of the light through the output mirror while reflecting a part of the remaining light by the output mirror. A w-axicon mirror is disposed at the other end of the cylindrical straight slab.

## Summary of the Invention

In a conventional cylindrical straight slab type gas laser employing such cylindrical straight slab does not exhibit preferable Gaussian distribution profile in beam intensity without operating the two cylindrical electrodes in accurate concentric relationship. As a result, a plurality of spacers are required to maintain accurate concentric relationship between the two cylindrical electrodes.

Unfortunately, however, the use of the spacers causes non-uniform beam profile which is impractical for a cutting machine because cutting width and cutting efficiency vary depending on the direction of movement of the beam.

It is, therefore, an object of the present invention to overcome the above problems of the prior art and to provide a slab type gas laser employing a cylindrical straight slab that eliminates the need for spacers for properly positioning the two cylindrical electrodes.

## Brief Description of Drawings

Now, the present invention will be described in greater detail by reference to the accompanying drawings, wherein :

FIG. 1 is a cross section view (A) and a side view (B) of one example of a conventional cylindrical straight slab type gas laser :

FIG. 2 shows a laser beam intensity distribution at the exit of an output mirror of a conventional laser :

FIG. 3 shows an intensity distribution of a far-field image of the laser beam as shown in FIG. 2 focused by a lens :

FIG. 4 is a simplified view of a first embodiment of the cylindrical straight slab type gas laser according to the present invention :

FIG. 5 is a laser beam intensity distribution at the exit of an output mirror of the laser as shown in FIG. 4 :

FIG. 6 shows laser beam intensity distributions of the far-field image of the laser beam as shown in FIG. 5 focussed by a lens : and

FIG. 7 is a cross section view of an important part of a second embodiment of the gas laser according to the present invention.

## Description of the Preferred Embodiments

For better understanding of the embodiments of the present invention, a conventional cylindrical straight slab type gas laser will be described first by reference to FIGs. 1-3. FIG. 1 (A) is a cross-section view and FIG. 1 (B) is a side view of a conventional cylindrical straight slab type gas laser. As illustrated in FIG. 1, the cylindrical straight slab type gas laser comprises a pair of concentrically and horizontally disposed cylindrical electrodes 11, 12 of different diameter. The gap between the two cylindrical electrodes 11, 12 is filled with laser medium to define a cylindrical straight slab 1. A ring-shaped trick mirror M1 is disposed at one end of the cylindrical straight slab 1. Also disposed at the center of the one end of the cylindrical straight slab 1 is an output mirror (half mirror) M2 to pass a part of the light through the output mirror while reflecting a part of the remaining light by the output mirror. A w-axicon mirror M3 is disposed at the other end of the cylindrical straight slab 1.

As mentioned above, the cylindrical straight slab type gas laser employing the cylindrical straight slab 1 may exhibit non-uniform split beam intensity distributions as shown in FIG. 3 (A) and (B) unless operated with accurate concentric positioning of the two cylindrical electrodes 11, 12. This is the reason why a plurality of spacers 13 are provided between the two cylindrical electrodes 11, 12 as illustrated in side view in FIG. 1. However, such spacers 13 cause beam intensity distribution with split peaks as shown in FIG. 2 at the exit of the output mirror M2.

When the laser beam is used in a cutting machine, any laser beam departing from the Gaussian distribution is impractical because cutting width and efficiency vary depending on the direction of

1 movement of the laser beam. This means that the spacers for maintaining the concentric relationship  
2 between the two cylindrical electrodes 11, 12 are obstacle to excellent laser beam profile.

3 The cylindrical straight slab type gas laser according to the present invention comprises two  
4 concentrically upstanding cylindrical electrodes of different diameter. The gap between the two  
5 cylindrical electrodes is filled with laser medium to define a cylindrical straight slab. A ring-shaped  
6 mirror is disposed at one end of the cylindrical straight slab. An output mirror is disposed at the center of  
7 the one end of the cylindrical straight slab to pass a part of the light through the output mirror while  
8 reflecting a part of the remaining light by the output mirror. A w-axicon mirror is disposed at the other  
9 end of the cylindrical straight slab to eliminate spacers between the two cylindrical electrodes.

10 (First Embodiment)

11 Now, illustrated in FIG. 4 is a simplified construction of the gas laser according to the present  
12 invention. The gas laser comprises a cylindrical straight slab 1 including a pair of vertically and  
13 concentrically disposed cylindrical electrodes 11, 12 of different diameter and laser medium filled in the  
14 gap between the two cylindrical electrodes 11, 12 to define a cylindrical straight slab 1. A ring-shaped  
15 trick mirror M1 is disposed at the top of the cylindrical straight slab 1 and also disposed at the top center of  
16 the cylindrical straight slab 1 is an output mirror (or half mirror) M2 to pass a part of the light through  
17 the output mirror and reflecting a part of the remaining light by the output mirror. Additionally, a w-  
18 axicon mirror M3 is disposed at the bottom of the cylindrical straight slab 1. This particular construction  
19 is effective to eliminate the need for spacers between the two cylindrical electrodes 11,12.

20 The outer cylindrical electrode 11, the ring-shaped trick mirror M1 and the w-axicon mirror M3 may be  
21 held in position by being supported to a frame of the device. On the other hand, the inner cylindrical  
22 electrode 12 extends at the upper end thereof to the inner circumferential surface of the ring-shaped trick  
23 mirror M1, thereby holding the upper end of the inner cylindrical electrode 12 on the inner surface of the  
24 trick mirror M1. The output mirror M2 may be held to the upper end of the inner cylindrical electrode 12.

25 When high frequency excitation voltage is applied between the cylindrical electrodes 11,12, the gas  
26 filled in the cylindrical straight slab 1 is excited to generate the laser beam by a resonator including the  
27 three mirrors M1, M2 and M3 and the laser beam is extracted from the output mirror M2.

28 The intensity distribution at the exit of the output mirror M2 is in the mode with aligned peak as  
29 shown in FIG. 5. The far-field image of the laser beam in this mode focused by a lens is a uniform beam  
30 close to Gaussian intensity distribution as shown in FIG. 6 (A) and (B) .

31 (Second Embodiment)

32 Positioning means for maintaining a pair of vertically disposed cylindrical electrodes 11, 12 in a  
33 concentric relationship is accomplished by making the cylindrical electrodes 11, 12 from ferro magnetic  
34 material and by magnetizing the material to have two or more permanent magnetic poles as illustrated in  
35 FIG. 7. The cylindrical permanent magnets are disposed in such a manner that inner and outer cylindrical

1 magnets repel to one another, thereby stably holding the two cylindrical electrodes 11, 12 in concentric  
2 manner.

3 As understood from the above description of the preferred embodiments, the gas laser according to the  
4 present invention can provide substantially uniform output beam close to Gaussian intensity distribution,  
5 which is suitable for a cutting machine. Since the concentric type straight slab laser is a diffused cooling  
6 type, there is no need for a circulation pump, thereby avoiding vibration and making the gas laser less  
7 expensive to make.

8 Although preferred embodiments of the cylindrical straight slab type gas laser according to the present  
9 invention are described herein, it is to be understood that the invention is not limited only to the above  
10 embodiments and that various modifications can be made by a person having an ordinary skill in the art  
11 without departing from the scope and spirit of the present invention. For example, the relationship  
12 between the cylindrical straight slab 1 and the mirrors M1~M3 may be inverted without changing the  
13 performance. In other words, the w-axicon mirror M3 is disposed at the top of the cylindrical straight slab  
14 1 while the ring-shaped trick mirror M1 and the output mirror (half mirror) M2 is disposed at the bottom  
15 of the cylindrical straight slab 1 .  
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